Impact Analysis of Headway Distribution on Single Lane Roundabout Entry Capacity

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Abstract

The Highway Capacity Manual (referred to as the HCM hereafter) 2000 model estimates roundabout entry capacity under an assumption of circulating headways following an exponential distribution. However, some studies indicated that the HCM 2000 model could over- or under-estimate entry capacity. This situation might be attributed to an unfit assumption of headway distribution type. Therefore, this study begins with analysis of headway distributions based on field survey. This study firstly indicates that the inverse Gaussian distribution is the best fitted distribution type of headway samples. According to this finding, we thus intend to adjust the HCM 2000 model. To this end, we propose a simulation based approach to estimate entry capacity of single-lane roundabouts. A linear relationship is established to represent the relationship between a capacity ratio of the simulation-based approach to the HCM 2000 model and conflicting flow. The linear function can be considered as a coefficient of the HCM 2000 model. It is believed that the modified HCM 2000 model outperforms the HCM 2000 model.

Keywords: headway distribution type analysis, modified HCM 2000 model, roundabout entry capacity.

Introduction

A roundabout is a type of circular intersection with one or more marked lanes in which road traffic is slowed and flows almost continuously in one direction around a central island to several exits onto the various intersecting roads (Hellinga and Sindi, 2012; Qu et al., 2014a). The early roundabouts are proposed a gyratory traffic scheme (*i.e.* one way circulation around a central island) (Qiu and Yin, 2011). Along with increase of traffic volume modern roundabouts are designed and established to satisfy higher requirements of safety, capacity and fluidity (Turner et al., 2011). Modern roundabouts have successfully implemented in Europe, Australia and the United States (Kittleson and Associates, 2011). Nowadays, roundabouts have been an increasingly popular intersection type, especially in less populous suburbs. In general, roundabouts substantially reduce queue and delay under low volume conditions as vehicles are not required to perform a complete stop. Roundabouts allow Uturn within the normal flow of traffic, which are often difficult to implement at other forms of junction (Flannery, 2011). Further, roundabouts provide higher safety than signal controlled junctions in terms of not only frequency but also severity of accidents. Fortuijn (2009) asserted that as the vehicles in a roundabout could drive along the same direction, the probability of crashes could be reduced thanks to the decrease of conflicting points. Along

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with the wider use of roundabouts, the entry capacity is of more importance to transport agencies (Bared and Afshar, 2009; Wei and Grenard, 2011).

Various models have been developed to estimate the entry capacities of roundabouts (Bie et al., 2012; Diah et al., 2011; Wong, 1996). Highway Capacity Manual (HCM) 2000 model is the most widely-used analytical model based on the gap acceptance theory (TRB, 2000), mathematically,

$$C_{2000} = v_c \times \frac{\exp(-v_c \tau_c / 3600)}{1 - \exp(-v_c \tau_f / 3600)}$$
(1)

where C_{2000} is the entry capacity of an arm (veh/hr); v_c is the conflicting circulating flow (veh/hr); τ_c and τ_f are critical gap and follow-up time (sec), respectively.

In the above-mentioned model, the entry capacity is calculated as a function of conflicting circulating flow, critical gap, and follow-up time. Additionally, the HCM 2000 model assumes that the circulating headways follow an exponential distribution (Polus et al., 2003; Wei and Grenard, 2012). However, some studies indicated that the HCM 2000 model may under- or over-estimate roundabout capacity (Mereszczak et al., 2006), and a relative error does exist in the HCM 2000 model (Cowan, 1997). Based on our research, follow-up time is possible to be measured from field survey. Furthermore, as critical gap cannot be observed directly, many feasible methods have been developed for its estimation from observed rejected and accepted gaps, such as those of Siegloch (1973), Raff (1950), Harder (1968) and Wu (2012). Accordingly, we conjecture that the relative error can be explained by an unrealistic assumption of headway distribution type. Hence, we intend to analyse impact of headway distribution type. To this end, this study begins with confirming a best fitted distribution type that circulating headways follow. Based on the accrual distribution types, we are able to modify the HCM 2000. In this study, we observed nine roundabouts (one hour per roundabout) to collect field survey data.

Data Collection

Based on field survey, nine roundabouts located in Gold Coast QLD, Australia are used to collect circulating headways, critical gaps and follow-up times at peak.

Headway

Headway is a time gap between two consecutive vehicles in circulating stream (Isebrand and Hallmark, 2012). As can be seen in Figure 1, headways are counted as time difference between two consecutive vehicles passing the red line.



Figure 1. A roundabout

Critical gap

The critical gap is estimated using the distributions of gap acceptance and rejection data. The methods commonly used for estimating the critical gap include the graphical method (Flannery and Datta, 1997; Siegloch, 1973), the maximum likelihood method (Harders, 1968; Raff and Hart, 1950; Troutbeck, 1992) and the probability equilibrium method (Wu, 2012). The graphical method is used in this study. The critical gaps are found to range from 4.32sec to 4.82 sec.

Follow-up Time

In this study, all follow-up times are measured from each roundabout. The follow-up time is then calibrated by taking a mean value of all measured follow-up times for each roundabout. They range between 2.35 sec and 2.75 sec.

Headway Distribution Type Analysis

As mentioned in introductory section, this study intends to analyse the distribution type of headways following. To this end, an engineering program, BestFit, is used to compare the histogram of headway samples and the probability of density function (PDF) of the exponential distribution. We then apply a Kolmogorov-Smirnov test (K-S test) to check whether headway samples follow an exponential distribution. The K-S test is a non-parametric test for the equality of continuous, one-dimensional probability distributions that can be used to compare a sample with a reference probability distribution (Jin et al., 2011; Meng and Qu, 2012; Qu et al., 2015; Qu and Meng, 2014). According to results from the BestFit and the K-S test, the majority of headway samples follow an inverse Gaussian distribution. In other words, inverse Gaussian distribution could be the best fitted distribution type of circulating headways following. The assumption of HCM 2000 model is not valid.

Model Improvement

As mentioned in the previous section, in most cases, the circulating headways do not follow exponential distributions. However, the HCM 2000 model provides an analytical solution to estimate roundabout entry capacity under an exponentially distributed assumption. In this study, we propose a simulation framework to estimate the entry capacities by taking into account the actual headway distributions.

Simulation Model

In this study, a simulation model is developed based on gap acceptance theory. According to drivers' decision making process, the number of vehicles being able to enter a roundabout could be formulated by

$$N = \begin{cases} 0, & \text{if } T < \tau_c \\ i, & \text{if } \tau_c + (i-1)\tau_f \le T < \tau_c + i\tau_f \end{cases}$$
(2)

where T is a time gap (headway) within circulating stream. Based on our field survey, various lengths of circulating headways are recorded for each roundabout. According to their corresponding calibrated critical gaps and follow-up times, the entry capacities for each roundabout can be estimated by summing numbers of vehicles being able to enter all headways in an hour. An example of the simulation is shown in Table 1. In the example, the calibrated critical gap and follow-up time are 4.61 sec and 2.39 sec, respectively.

| Table 1. An example of the simulation | | | | | | | | | | | |
|---------------------------------------|-----------|------------------------|-------------|--------------------|--|--|--|--|--|--|--|
| Cumulative | Headways, | Simulated No. of | No. of | Simulated Capacity | | | | | | | |
| time (sec) | T (sec) | vehicles entering, N | headways, n | (veh/hr) | | | | | | | |
| 0 | 0 | 0 | 0 | 1248 | | | | | | | |
| 23.273 | 23.273 | 8 | 1 | | | | | | | | |
| 58.363 | 35.09 | 13 | 2 | | | | | | | | |
| 59.937 | 1.574 | 0 | 3 | | | | | | | | |
| 68.212 | 8.275 | 2 | 4 | | | | | | | | |
| 71.475 | 3.263 | 0 | 5 | | | | | | | | |
| 78.018 | 6.543 | 1 | 6 | | | | | | | | |
| 92.302 | 14.284 | 5 | 7 | | | | | | | | |
| 108.758 | 16.456 | 5 | 8 | | | | | | | | |
| 146.738 | 37.98 | 14 | 9 | | | | | | | | |
| 158.907 | 12.169 | 4 | 10 | | | | | | | | |
| 202.453 | 43.546 | 17 | 11 | | | | | | | | |
| | | | | | | | | | | | |
| 3596.479 | 12.458 | 4 | 257 | | | | | | | | |
| 3600.024 | 3.545 | 0 | 258 | | | | | | | | |

Notes: Headway = cumulative time_{*n*} - cumulative time_{*n*-1}, $\forall n \in (1, 258)$

Conflicting flow, $v_c = No.$ of headways (258 veh / hr)

Simulated capacity =
$$\sum_{n=1}^{n=258} N$$

Similarly, the entry capacities for the other eight roundabouts are estimated, ranging from 514 to 1248 veh/hr.

A Comparison between the Results from the Simulation Model and HCM 2000 Model To modify the HCM 2000 model, we establish a linear function as a coefficient based on a regression analysis. In this study, all data for the regression analysis, including critical gaps, follow-up times and conflicting flows, are collected from nine observed roundabouts. For establishing the linear function, the following procedure is recommended:

- 1. Calibrate conflicting flow for one roundabout using the introduced simulated method in Table 1.
- 2. Based on its calibrated critical gap and follow-up time and conflicting flow, calculate entry capacity according to the HCM 2000 model using Eqn. (1).
- 3. Estimate entry capacity according to the simulation in Table 1.
- 4. Calculate a capacity ratio of the simulation to the HCM 2000 model.
- 5. Repeat step 1 to 4 and calculate capacity ratios for all nine observed roundabouts. Capacity ratios are shown in Table 2.

According to nine capacity ratios, establish a linear function which is shown in Figure 2.

| Roundabout (i) | Conflicting | Capacity (veh/hr) | | Datio | Calibrated | Modified HCM | Relative error (%) | | RMSD | |
|-------------------|------------------|-------------------|-------------|------------------|------------|----------------------|--------------------|-----------------|-------------|-----------------|
| | flow (veh/hr) | Simulation | HCM 2000 | (Simulation/HCM) | ratio | capacity (veh/hr) | HCM 2000 | Modified HCM | HCM 2000 | Modified HCM |
| 1 | 249 | 1202 | 1208 | 0.9950 | 1.0069 | 1216 | 4.66 | 0.92 | 48.17 | 12.79 |
| 2 | 220 | 1248 | 1222 | 1.0213 | 1.0185 | 1245 | | | | |
| 3 | 258 | 1150 | 1135 | 1.0132 | 1.0033 | 1139 | | | | |
| 4 | 291 | 1099 | 1081 | 1.0167 | 0.9901 | 1070 | | | | |
| 5 | 744 | 514 | 634 | 0.8107 | 0.8089 | 513 | | | | |
| 6 | 378 | 968 | 1014 | 0.9546 | 0.9553 | 969 | | | | |
| 7 | 409 | 924 | 972 | 0.9506 | 0.9429 | 916 | | | | |
| 8 | 310 | 1002 | 1030 | 0.9728 | 0.9825 | 1012 | | | | |
| 9 | 248 | 1113 | 1117 | 0.9964 | 1.0073 | 1125 | | | | |

Table 2. HCM 2000 model calibration and validation

Notes: Calibrated ratio = $-0.0004v_c + 1.1065$

Modified HCM capacity = Calibrated ratio \times HCM 2000

Relative error_{HCM 2000} = 100% ×
$$\left(\sum_{i=1}^{i=9} \left| \frac{\text{HCM 2000}_i - \text{Simulation}_i}{\text{Simulation}_i} \right| \right) / 9$$

Relative error_{Modified HCM} = 100% × $\left(\sum_{i=1}^{i=9} \left| \frac{\text{Modified HCM}_i - \text{Simulation}_i}{\text{Simulation}_i} \right| \right) / 9$

RMSD is root-mean-square deviation

$$RMSD_{HCM 2000} = \sqrt{\frac{\sum_{i=1}^{100} \left[(HCM 2000_{i} - Simulation_{i})^{2} \right]}{9}}$$
$$RMSD_{Modified HCM} = \sqrt{\frac{\sum_{i=1}^{100} \left[(Modified HCM_{i} - Simulation_{i})^{2} \right]}{9}}$$



Figure 2. Trendline of capacity ratio

As can be seen in Figure 2, a linear trendline is found to show the relationship between the capacity ratio of the simulation to the HCM 2000 model and conflicting flow. The linear trendline represents a function to modify the HCM 2000 model as follows:

Calibrated ratio =
$$-0.0004v_c + 1.1065$$
 (3)

Additionally, the HCM 2000 model can be then modified as follows:

$$C_m = (-0.0004v_c + 1.1065) \times C_{2000} \tag{4}$$

where C_m is the entry capacity from the modified HCM 2000 model.

In this study, we thus validate the modified HCM 2000 model. As can be seen in Table 2, the modified HCM 2000 model provides a smaller value of relative error (0.92%) and RMSD (12.79) than the HCM 2000 model (4.66% and 48.17). Accordingly, the modified HCM 2000 model is proven outperform the HCM 2000 model. This finding successfully validates the feasibility of the modified HCM 2000 model.

Conclusion

Some studies asserted that the HCM 2000 model could over- or under- estimate singlelane roundabout entry capacity because an unfit assumption of headway distribution type is used. Accordingly, this study firstly analyses headway distributions based on field survey. It is found that the inverse Gaussian distribution is the most suitable distribution type of headway samples. According to this finding, this paper adjusts the HCM model by proposing a simulation based approach to estimate entry capacity. A linear relationship is thus established to represent the relationship between a capacity ratio of the simulationbased approach to the HCM 2000 model and conflicting flow. The linear function can be considered as a coefficient of the HCM 2000 model. It is believed that the modified HCM 2000 model outperforms the HCM 2000 model.

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